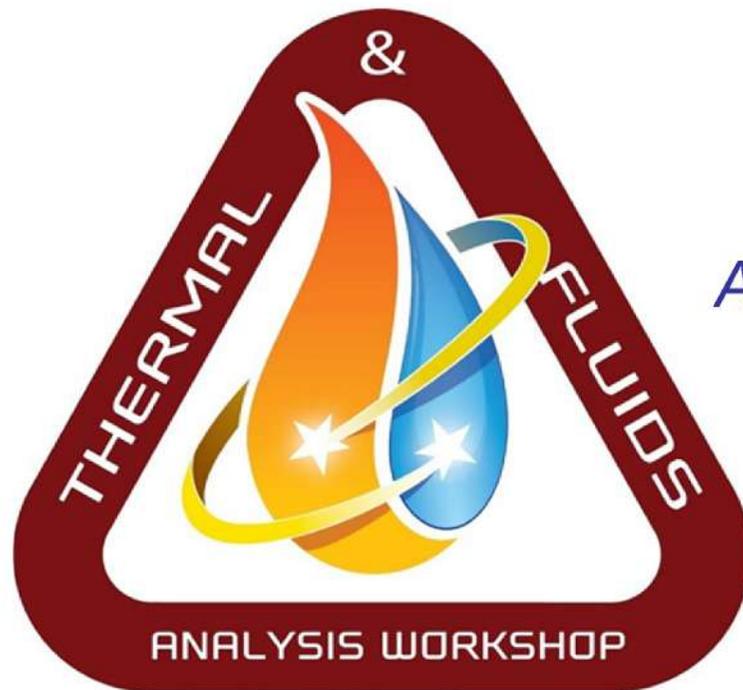




Cubesats: A passive thermal analysis approach

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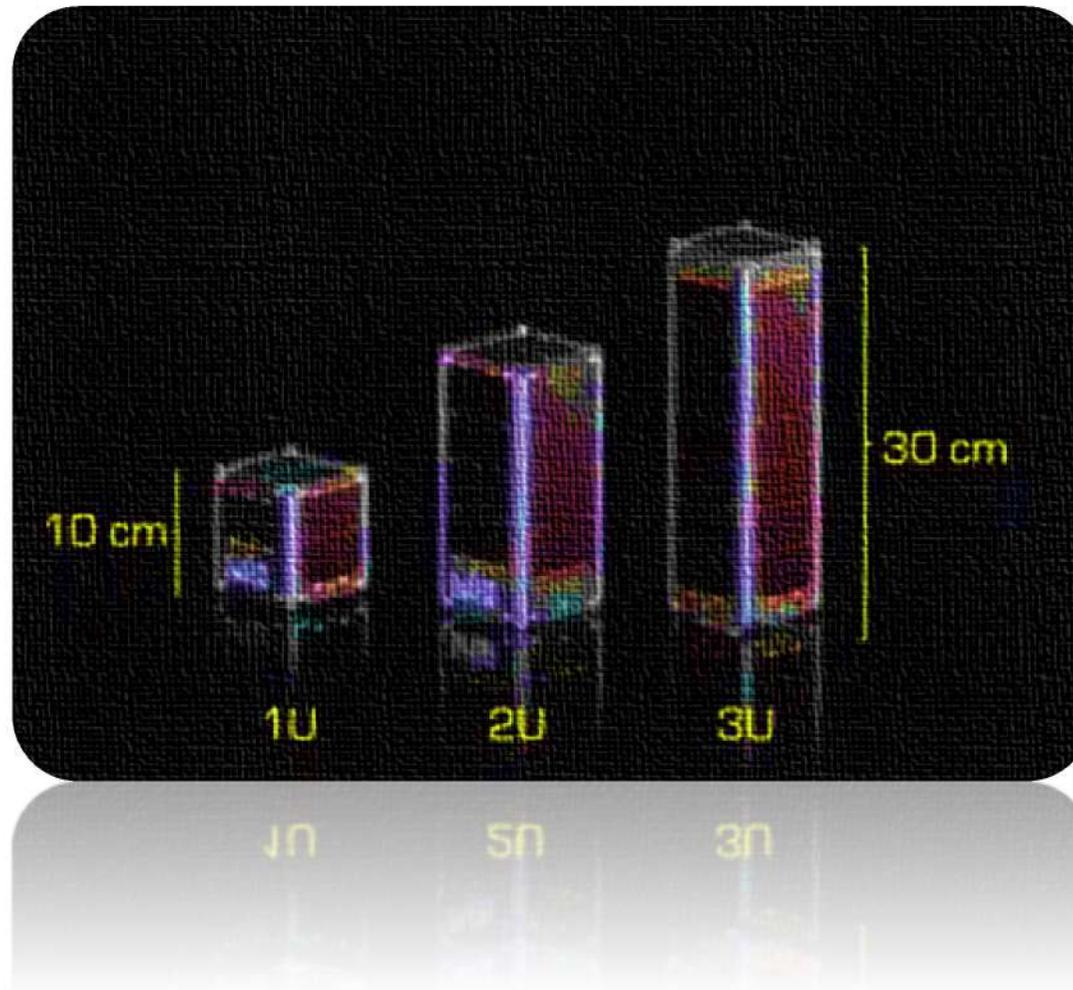


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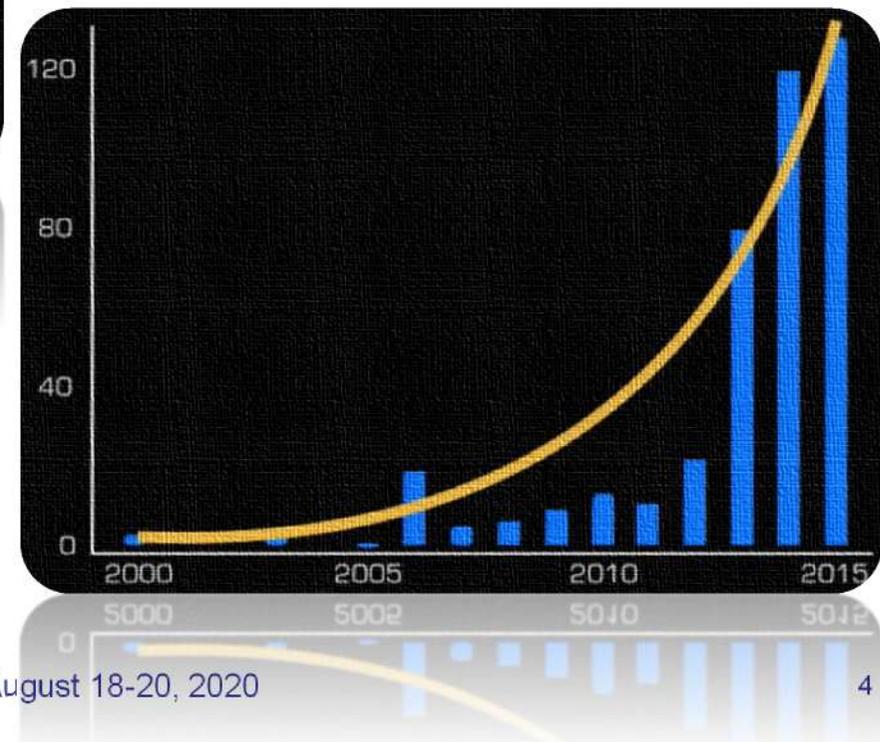
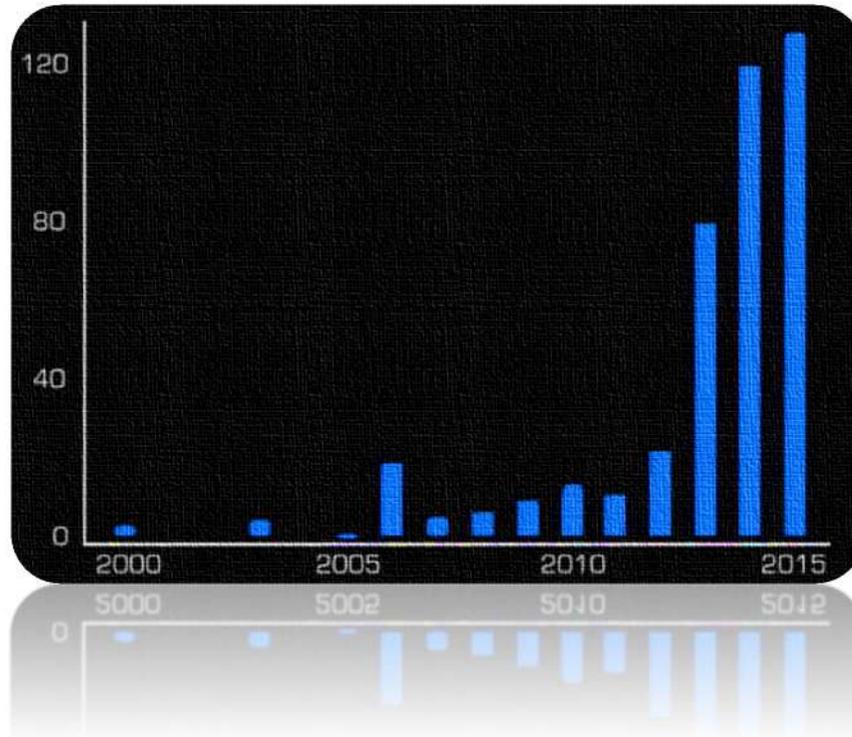


- Introduction
- Context and objectives
- Methodologies
- Results
- Conclusion

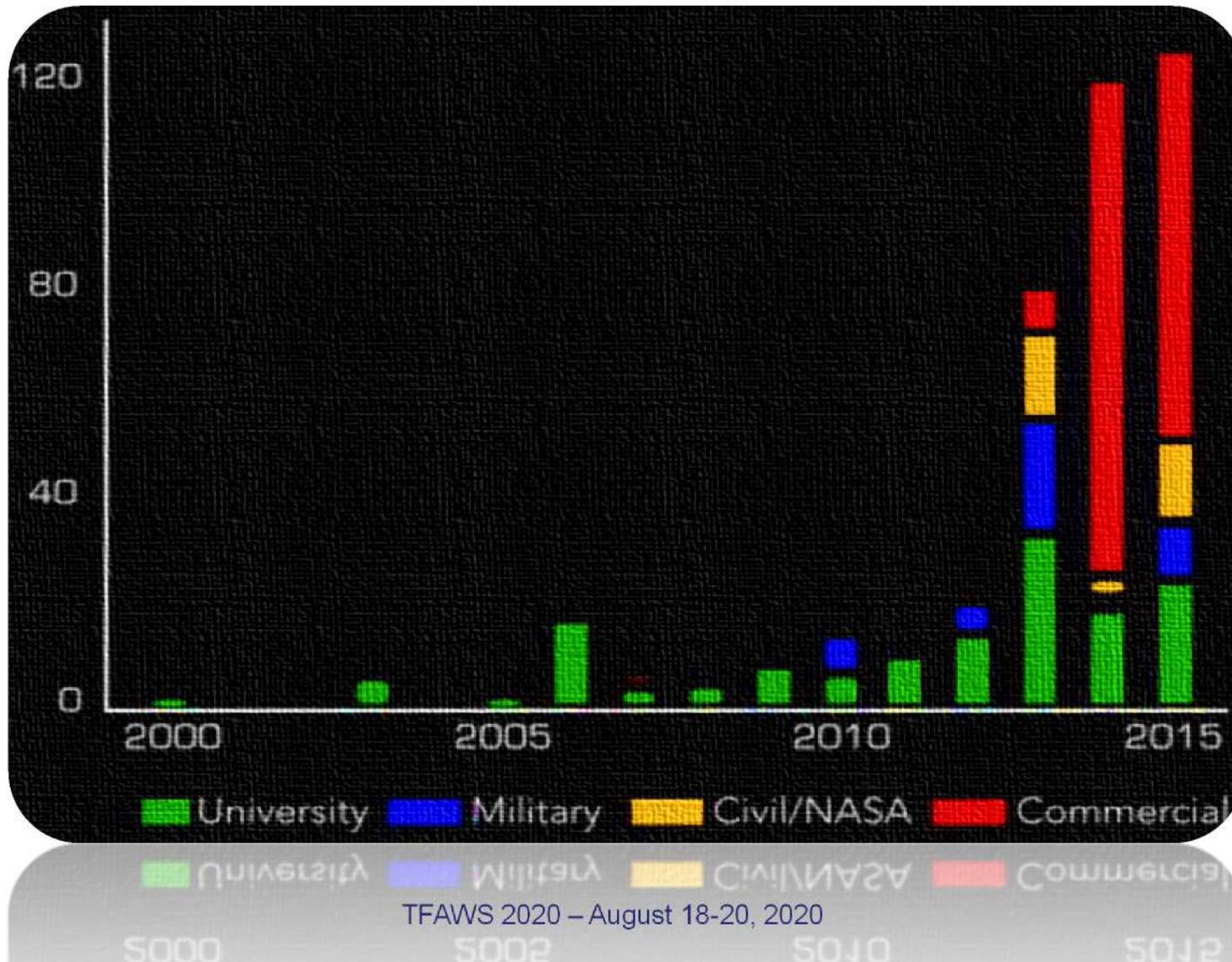
A brief reminder



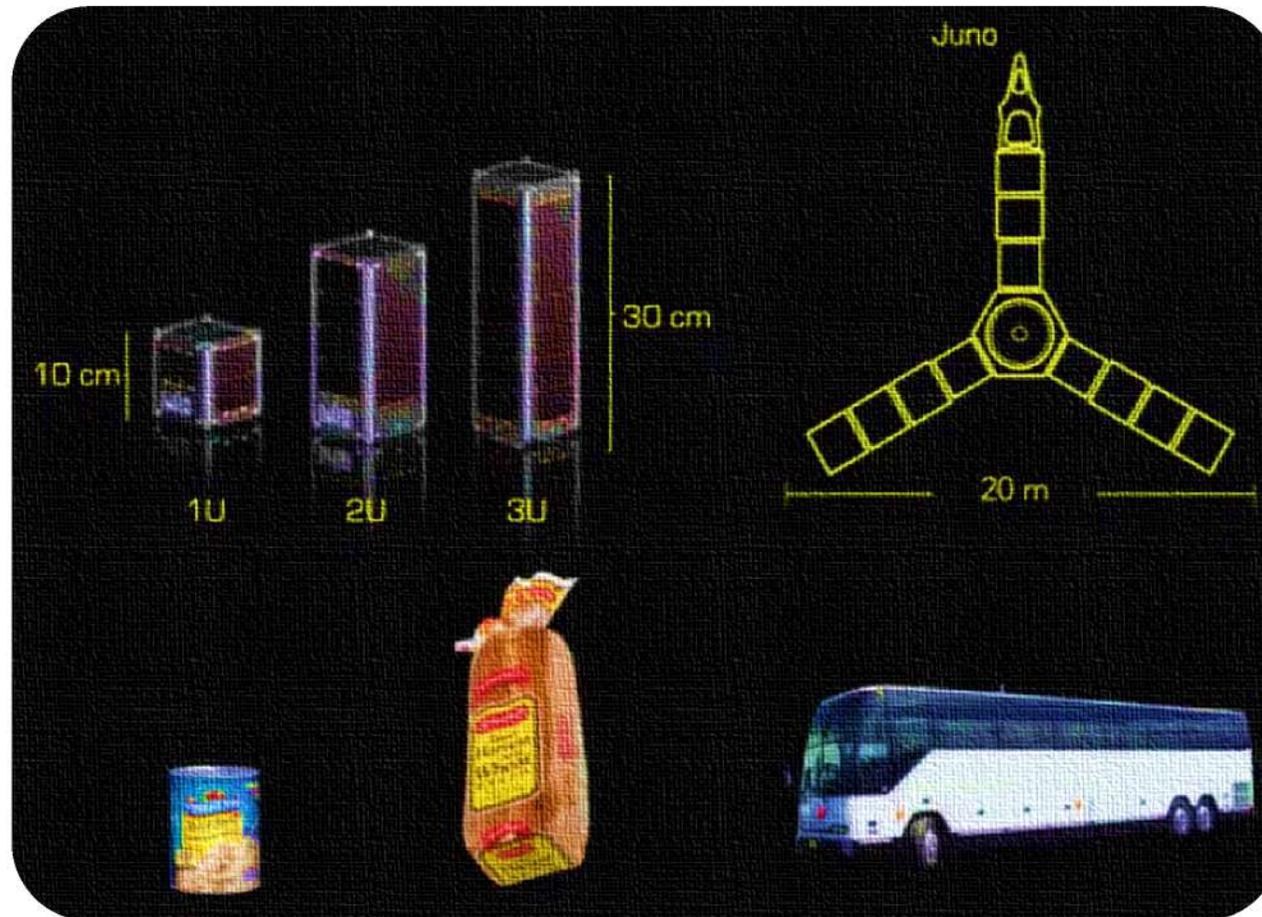
Cubesats launched since 2000



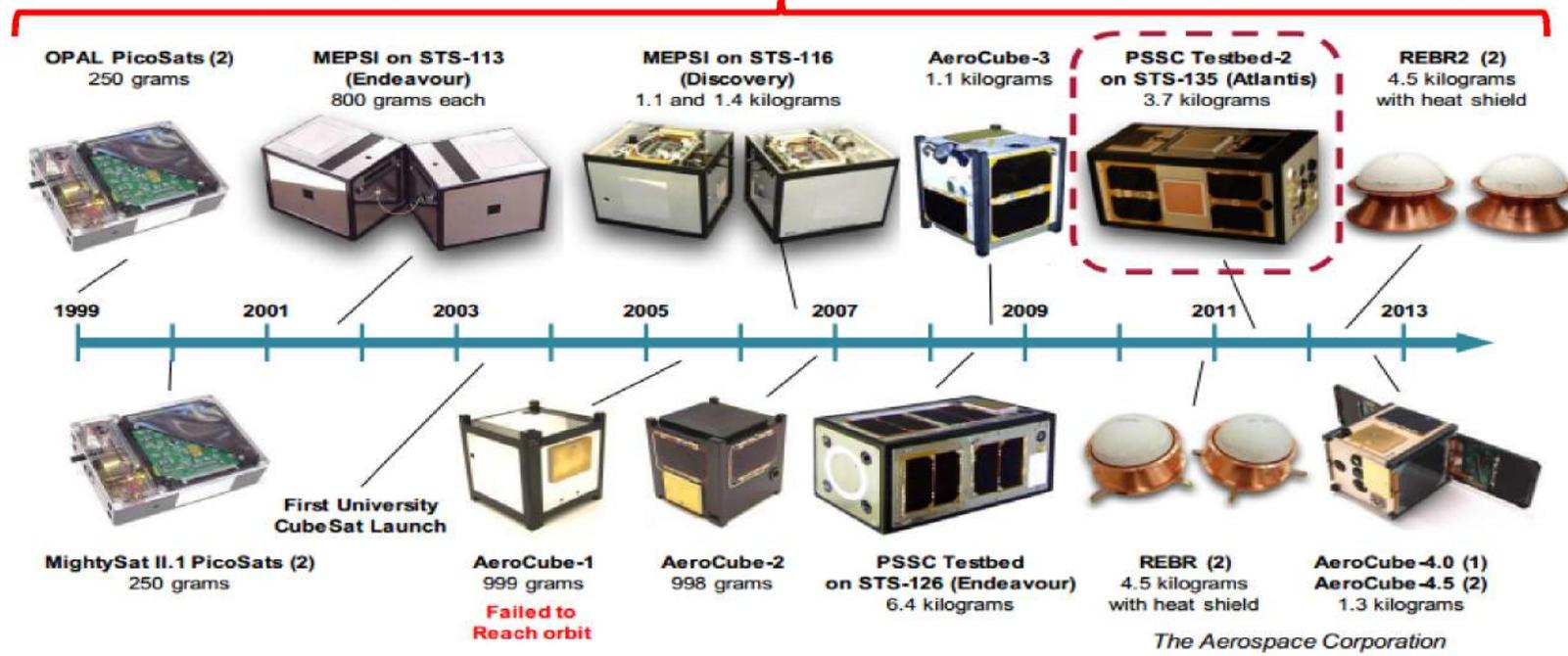
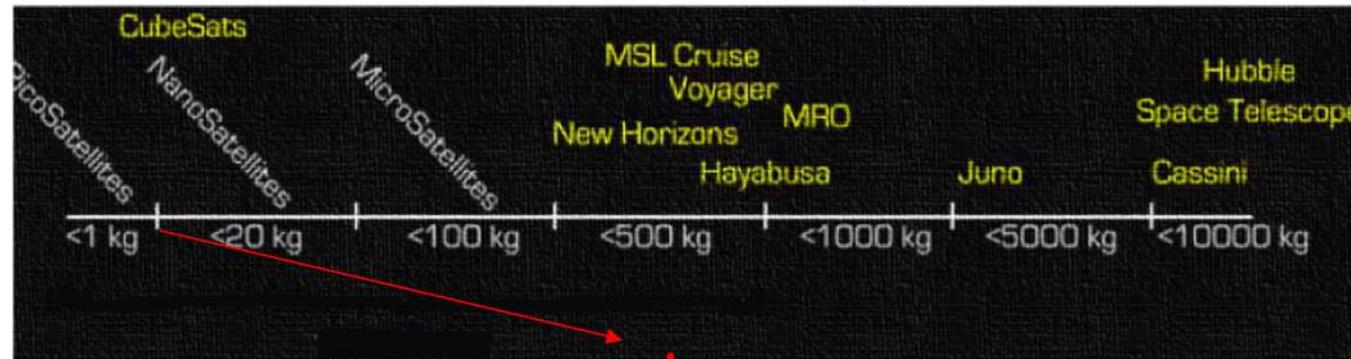
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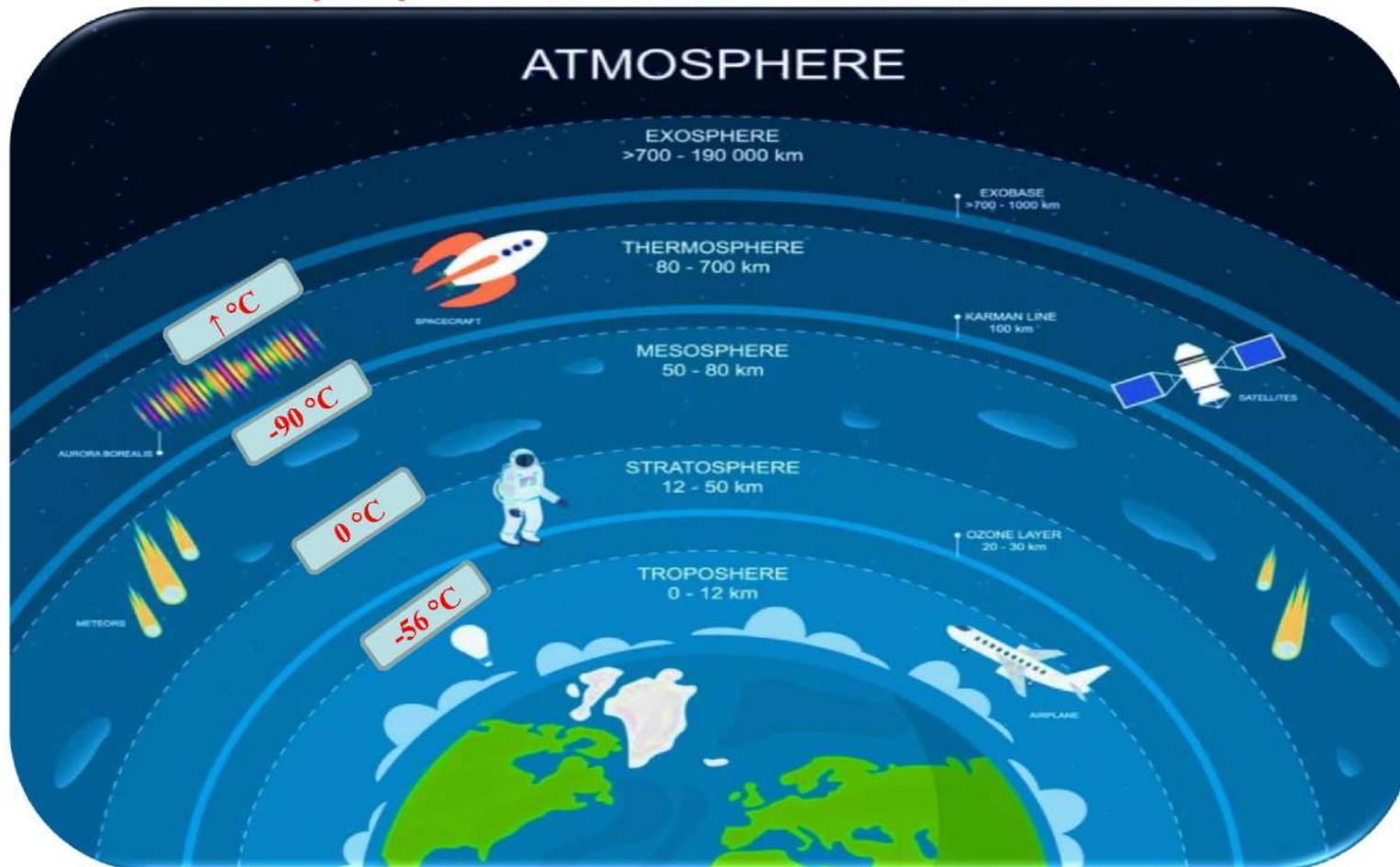
Idea about what Cubesats look like...



Cubesats weight



The purpose of satellite thermal control?

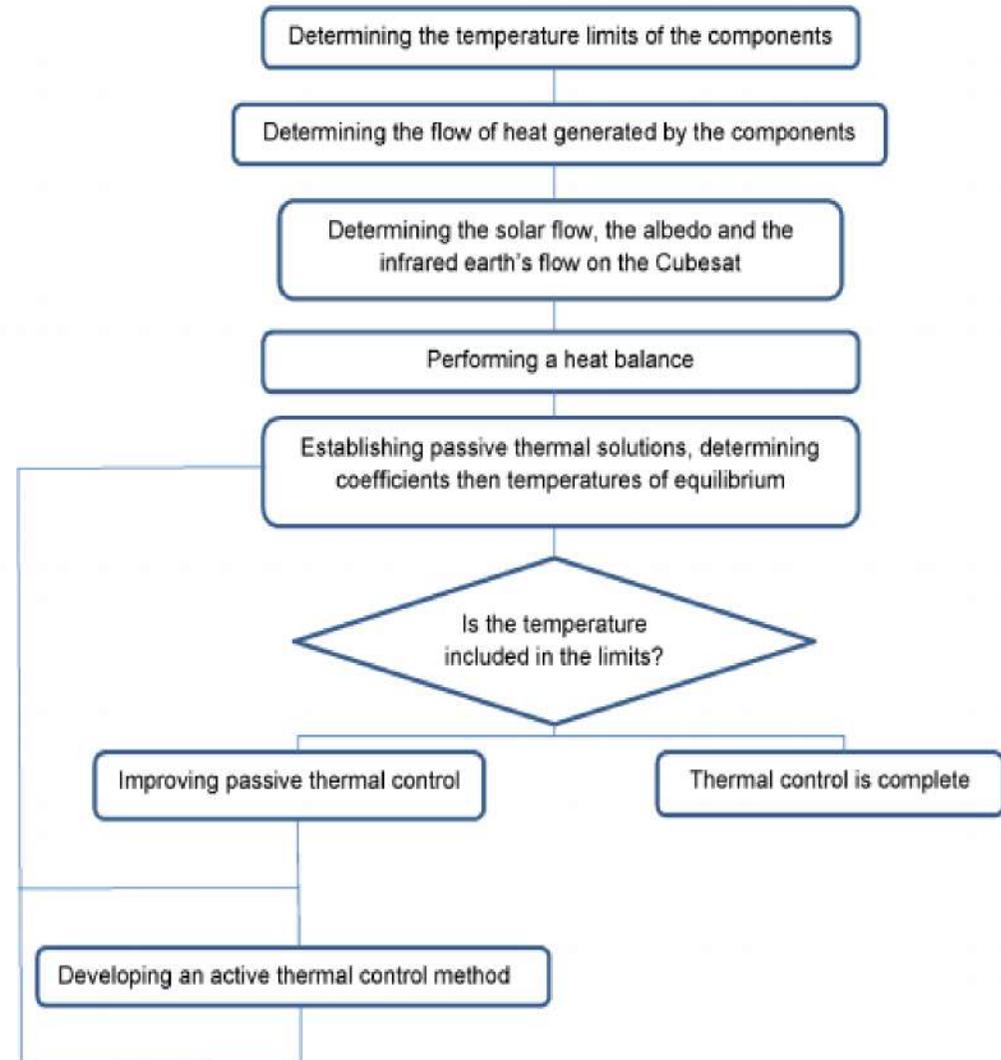


- *Adapting exchanges with the environment to ensure a suitable average temperature*
- *Playing on internal exchanges to facilitate the evacuation of internally dissipated powers*

There are two types of thermal control:

- **Passive thermal control** which attempts, by means of passive devices (paintings, multi-layer insulation, reflectors, etc.) to control heat transfers that are carried out by conduction and thermal radiation. It is a less expensive, lightweight, reliable solution with little impact on mass and power estimation.
- **Active thermal control** which is often justified by the uncertainties of the model, the variable environment and the aging of the microsatellite.

Passive thermal flow chart

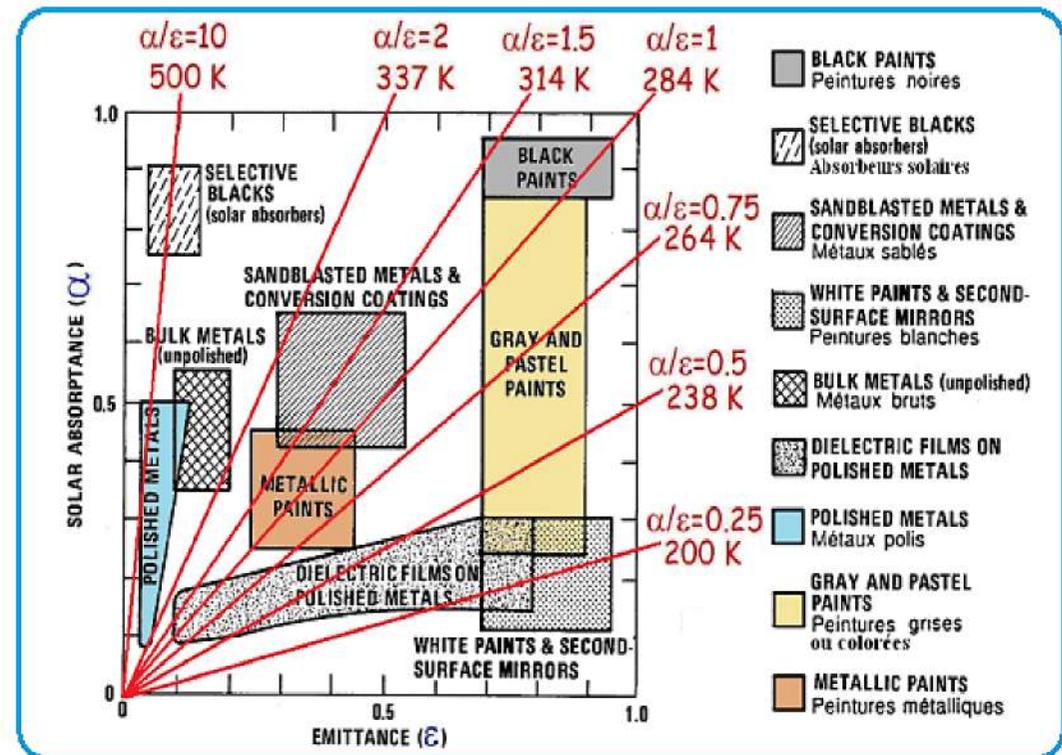


Means of controlling radiative exchanges

The temperature of a body in space depends heavily on the thermo-optical characteristics of its coatings: Solar Absorptivity α and IR emissivity ε .

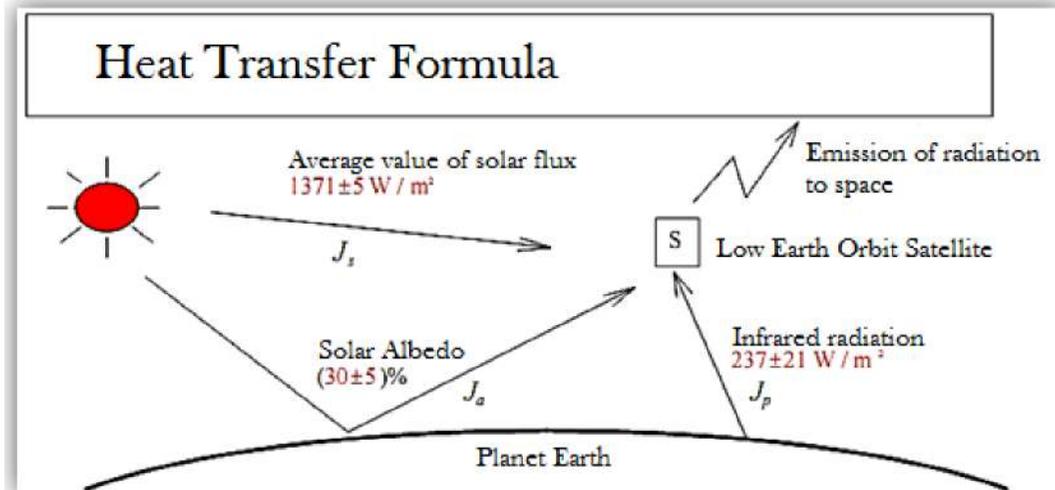
If we consider the ratio α/ε as a criterion, these coatings can be classified into four categories :

- Cold coatings with low $\alpha / \varepsilon < 1$: White paint.
- Average coatings at $\alpha / \varepsilon \sim 1$: Black paint.
- Hot coatings at $\alpha / \varepsilon > 1$: Polished golden aluminum.
- Super hot coatings at $\alpha / \varepsilon > 4$: Black chrome.



Thermal analysis process

The main heat source when the Cubesat is in orbit is the Photosphere, the thermal transfer is governed by :



$$\sigma A_{Sat} \epsilon T^4 = \begin{aligned} & Q_i && \text{(Internal flow)} \\ & + \alpha J_s A_{Sun} && \text{(Solar radiation)} \\ & + \alpha J_a A_{albedo} && \text{(Reflected Solar radiation)} \\ & + \epsilon J_p A_{Earth} && \text{(Infrared Terrestrial radiation)} \end{aligned}$$

(Thermal emission)

Assumptions and boundary conditions

The expression of the calculation of the temperature is :

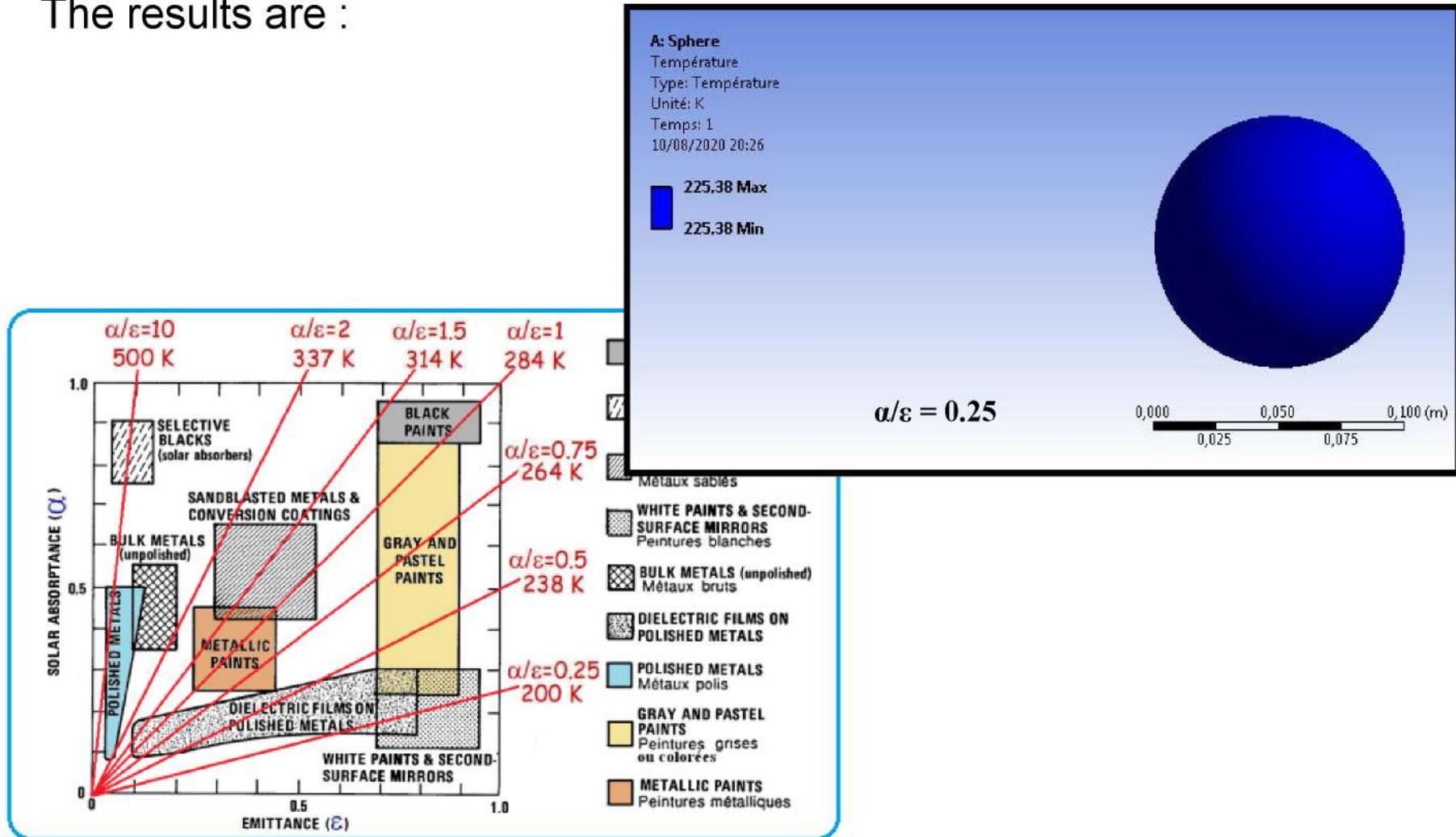
$$T^4 = \frac{A_{Earth} J_p}{A_{Sat} \sigma} + \frac{Q_i}{A_{Sat} \sigma \epsilon} + \left[\frac{A_{Sun} J_s}{A_{Sat} \sigma} + \frac{A_{albedo} J_{albedo}}{A_{Sat} \sigma} \right] \times \frac{\alpha}{\epsilon}$$

With,

- Circular dawn-dusk Orbit is a near-polar orbit at low altitude, which does not suffer from eclipses.
- J_s , J_a , J_p and Q_i are constant.
- The sidereal temperature is 2,7K.
- The solar flux, the albedo and the infrared terrestrial flux reach the nanosatellite perpendicularly.
- The nanosatellite is considered to be a real body.
- Orbit at 240Km
- $J_s = 1371 \text{ W/m}^2$
- $J_a = 67,8645 \text{ W/m}^2$
- $J_p = 220 \text{ W/m}^2$
- $Q_i = 0 \text{ W/m}^2$

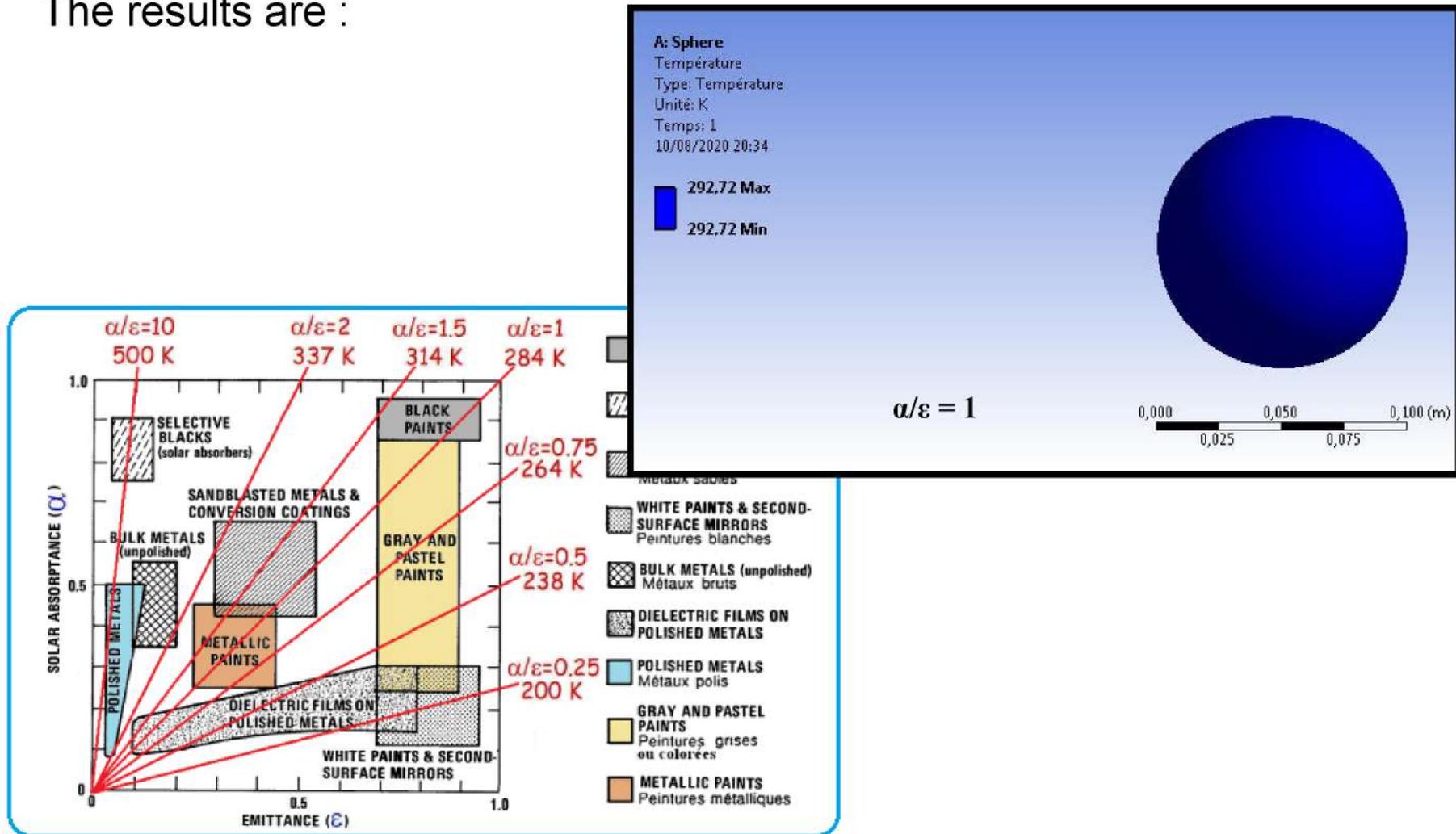
System validation

The results are :



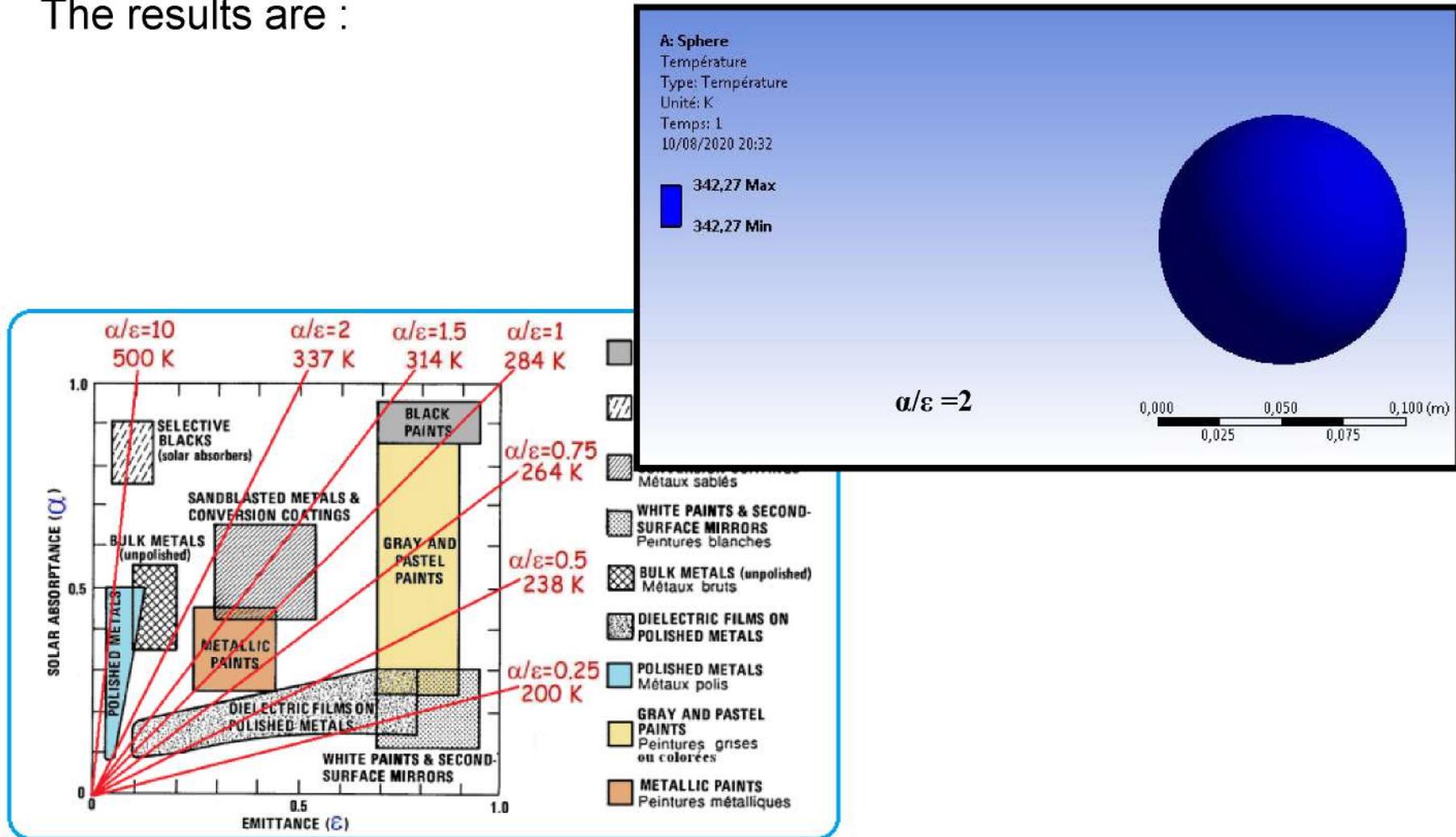
System validation

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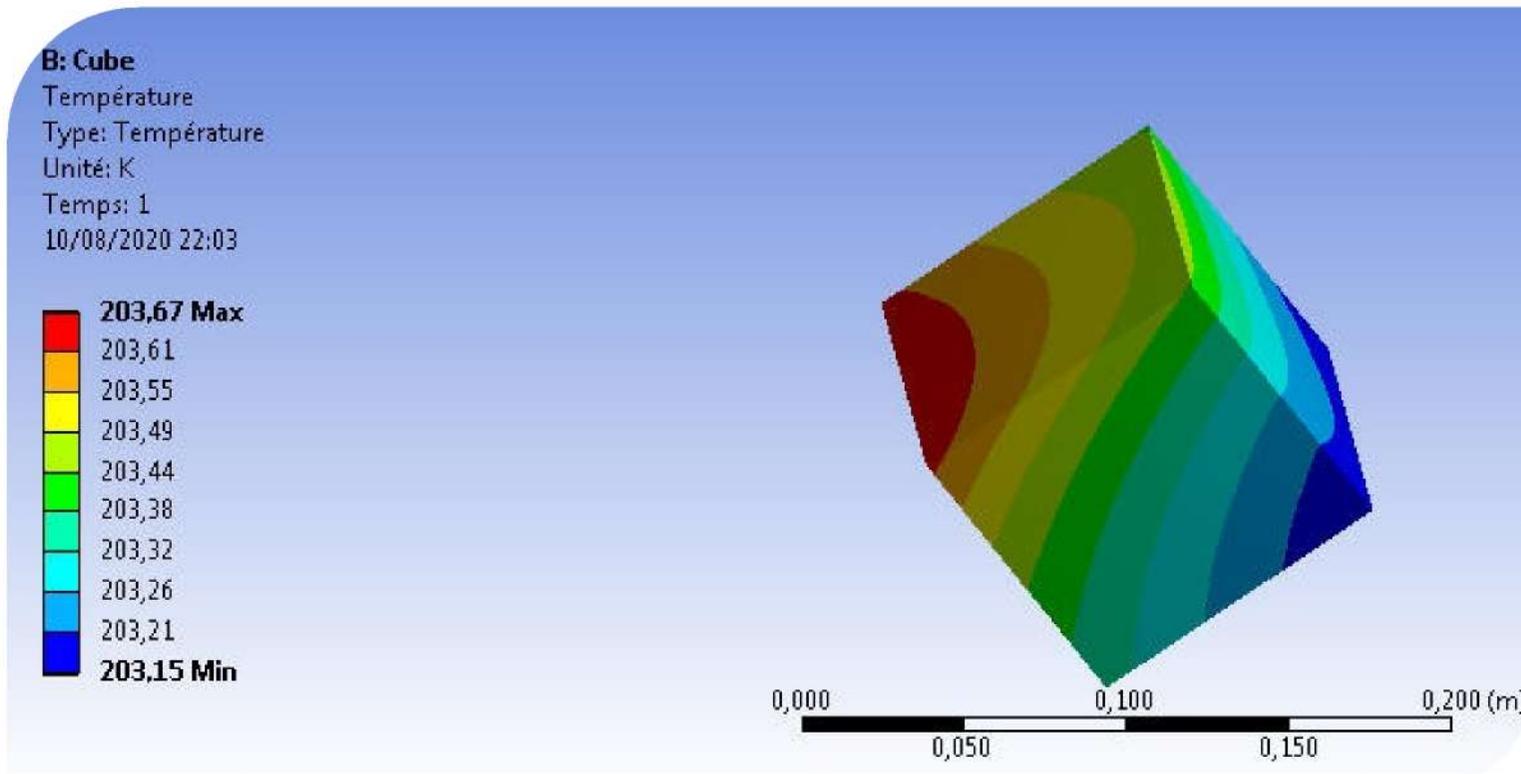
System validation

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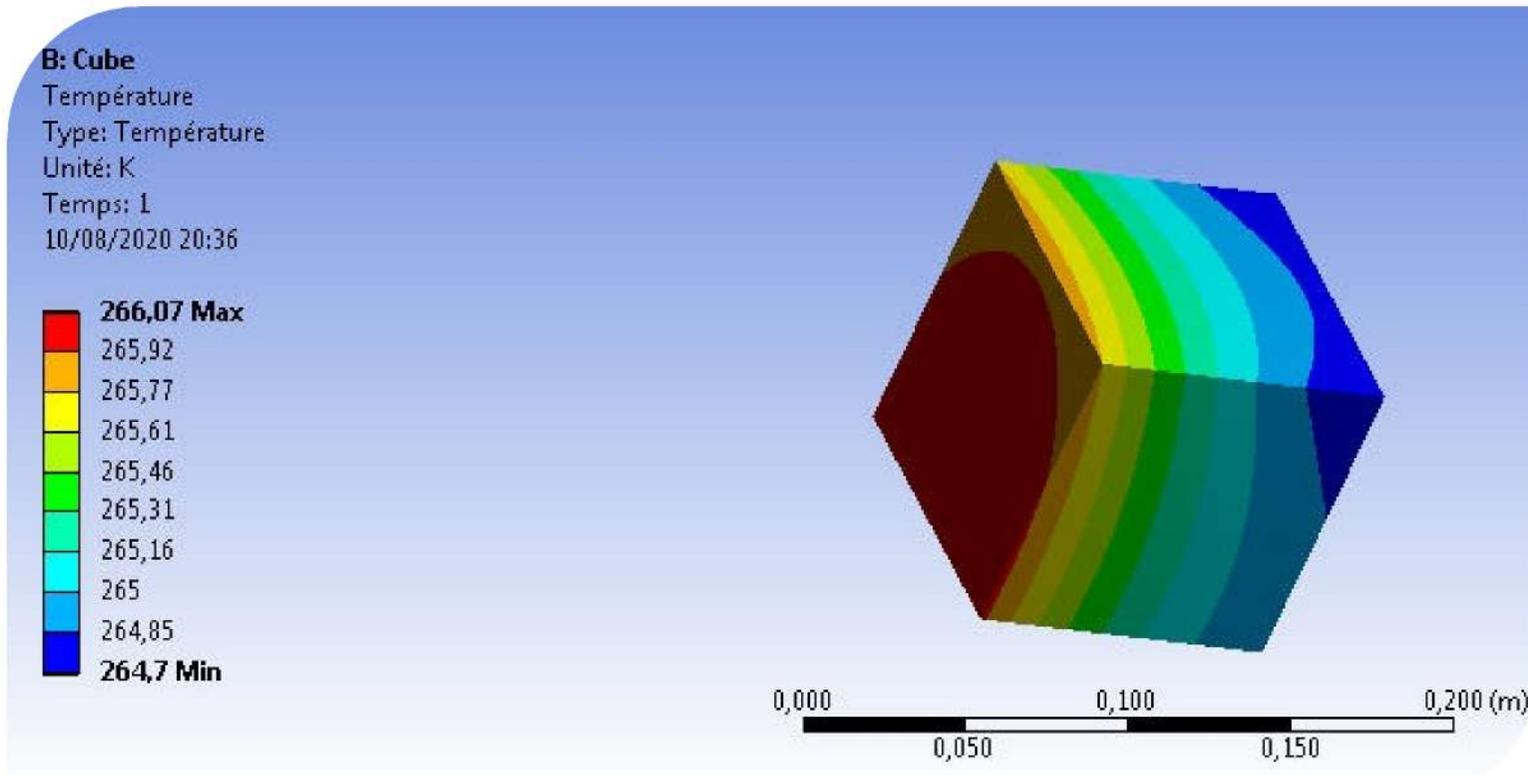
Cubesat analysis “Steady state”

- $\alpha/\varepsilon = 0.25$; $T = -69.483 \text{ }^\circ \text{C} \sim -70.001 \text{ }^\circ \text{C}$



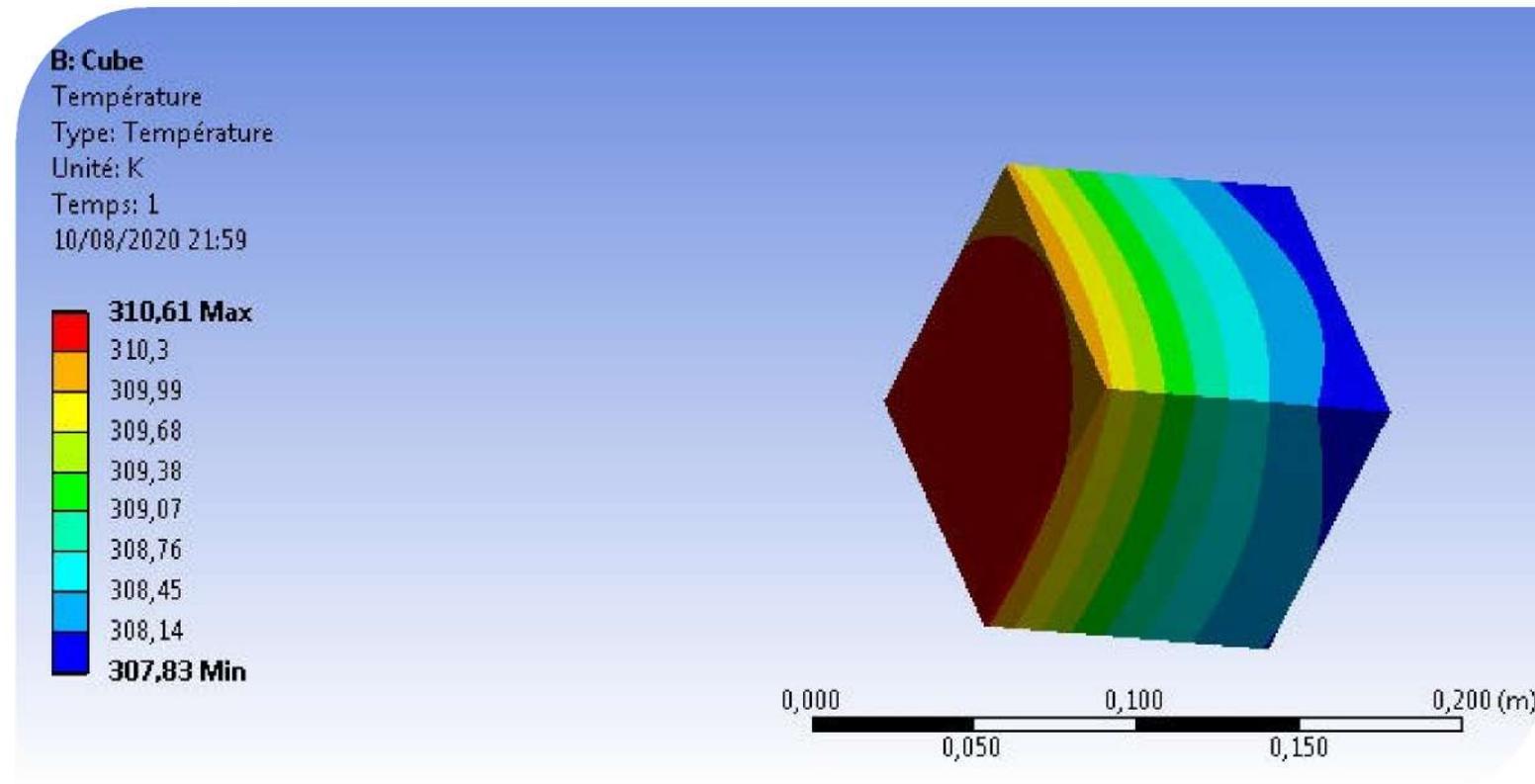
Cubesat analysis “Steady state”

- $\alpha/\varepsilon = 1$; $T = -7.07^\circ \text{ C} \sim -8.45^\circ \text{ C}$



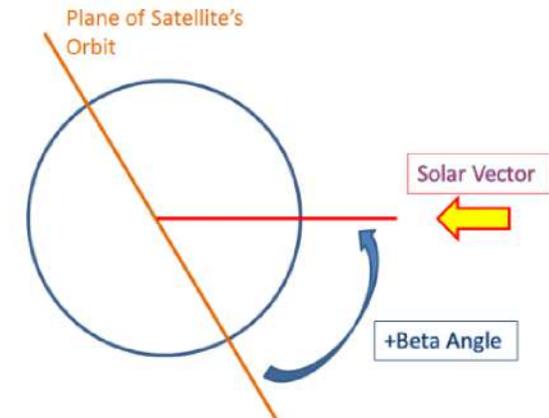
Cubesat analysis “Steady state”

- $\alpha/\varepsilon = 2$; $T = 37.41^\circ \text{ C} \sim 34.63^\circ \text{ C}$



Cubesat analysis “Transient state”

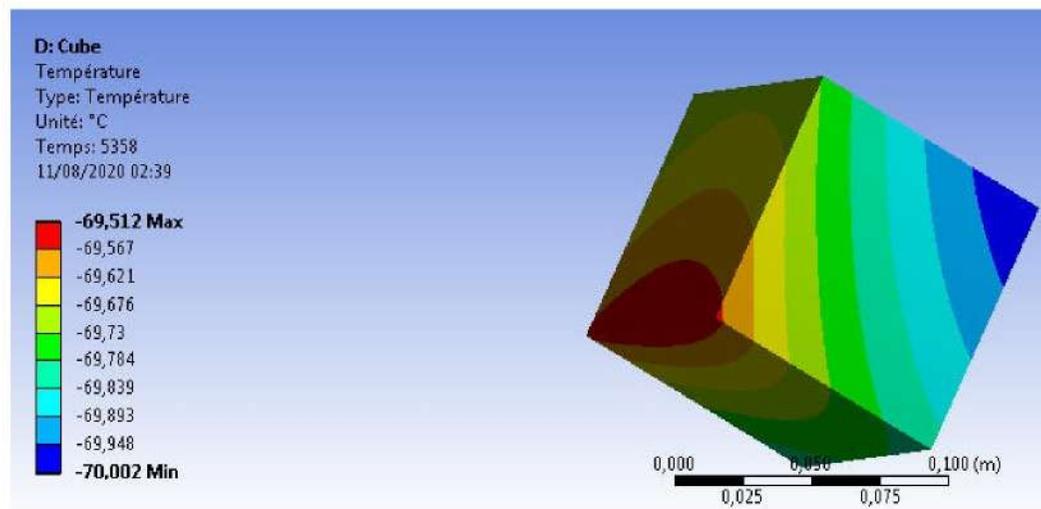
- For transient analysis, some parameters should be defined :
- Beta Angle is still positive while revolving (Counter clock revolution).
- $R_{\text{Earth}} = 6378 \text{ Km}$
- $H = 240 \text{ Km}$
- Orbit's semi major axis $a = H + R_{\text{Earth}} = 6618 \text{ Km}$
- Gravitational parameter $\mu = 3.986 \cdot 10^5 \text{ Km}^3/\text{s}^2$
- Period revolution $P = 2 \cdot \pi \cdot (a^3/\mu)^{0.5} = 5358 \text{ s}$
- Number of periods per day $n = (3600 \cdot 24)/P = 16 \text{ Rev/day}$
- Velocity $v = (\mu/a)^{0.5} = 7.76 \text{ Km/s}$



Cubesat analysis “Transient state”

- $\alpha/\varepsilon = 0.25$; [T = -69.48° C ~ -70.00° C] Steady state Temperature
 →→ [T_{moy} = -69.74° C] Initial Temperature injected in Transient analysis

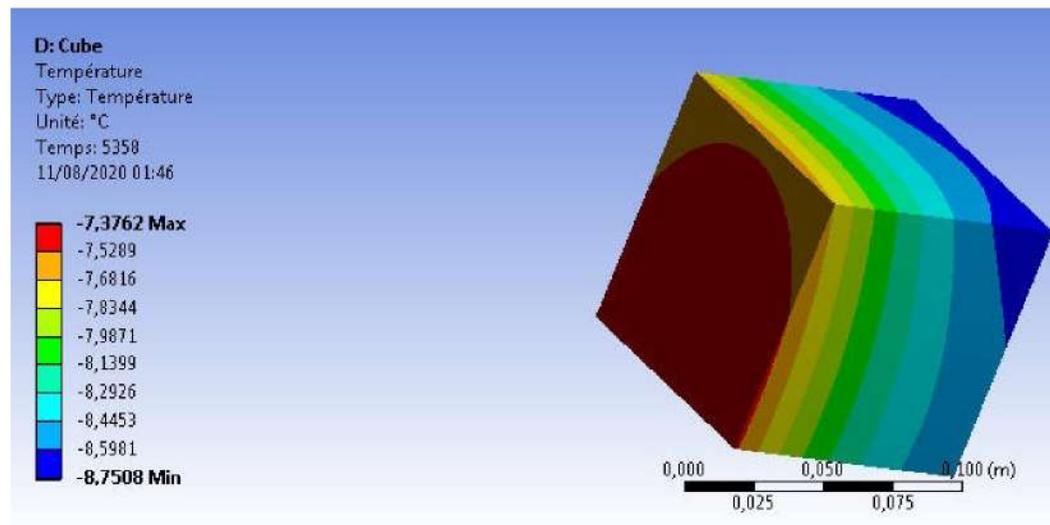
P	1	2	3	4	5	6	7	8	9
Tmax	-69.51	-69.52	-69.53	-69.54	-69.55	-69.56	-69.57	-69.58	-69.59
Tmin	-70	-70.01	-70.02	-70.03	-70.04	-70.05	-70.06	-70.07	-70.08



Cubesat analysis “Transient state”

- $\alpha/\varepsilon = 1$; [T = -7.07° C ~ -8.45° C] Steady state Temperature →→
 →→ [T_{moy} = -7.76° C] Initial Temperature injected in Transient analysis

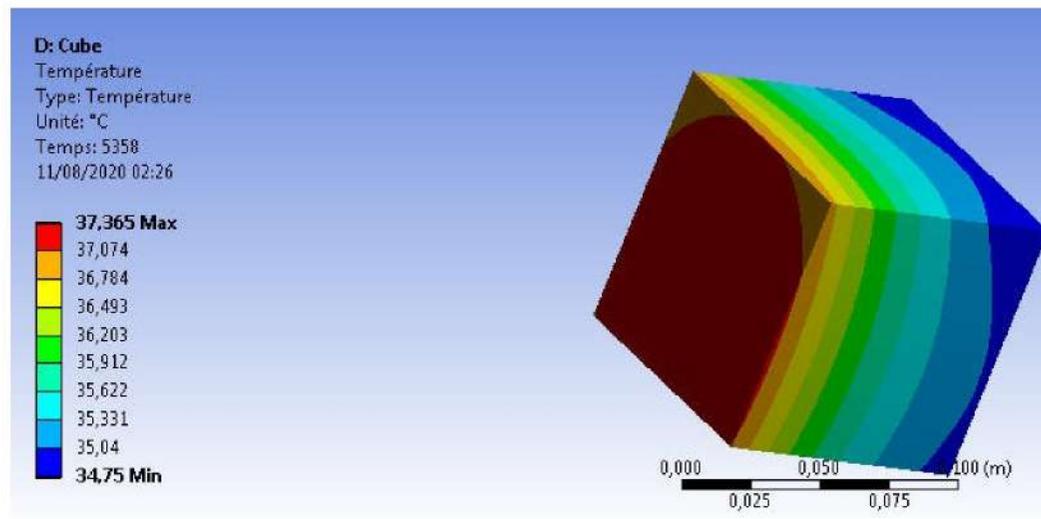
P	1	2	3	4	5	6	7	8	9
Tmax	-7.37	-7.58	-7.71	-7.8	-7.87	-7.91	-7.94	-7.96	-7.97
Tmin	-8.75	-8.95	-9.09	-9.18	-9.24	-9.28	-9.31	-9.33	-9.34

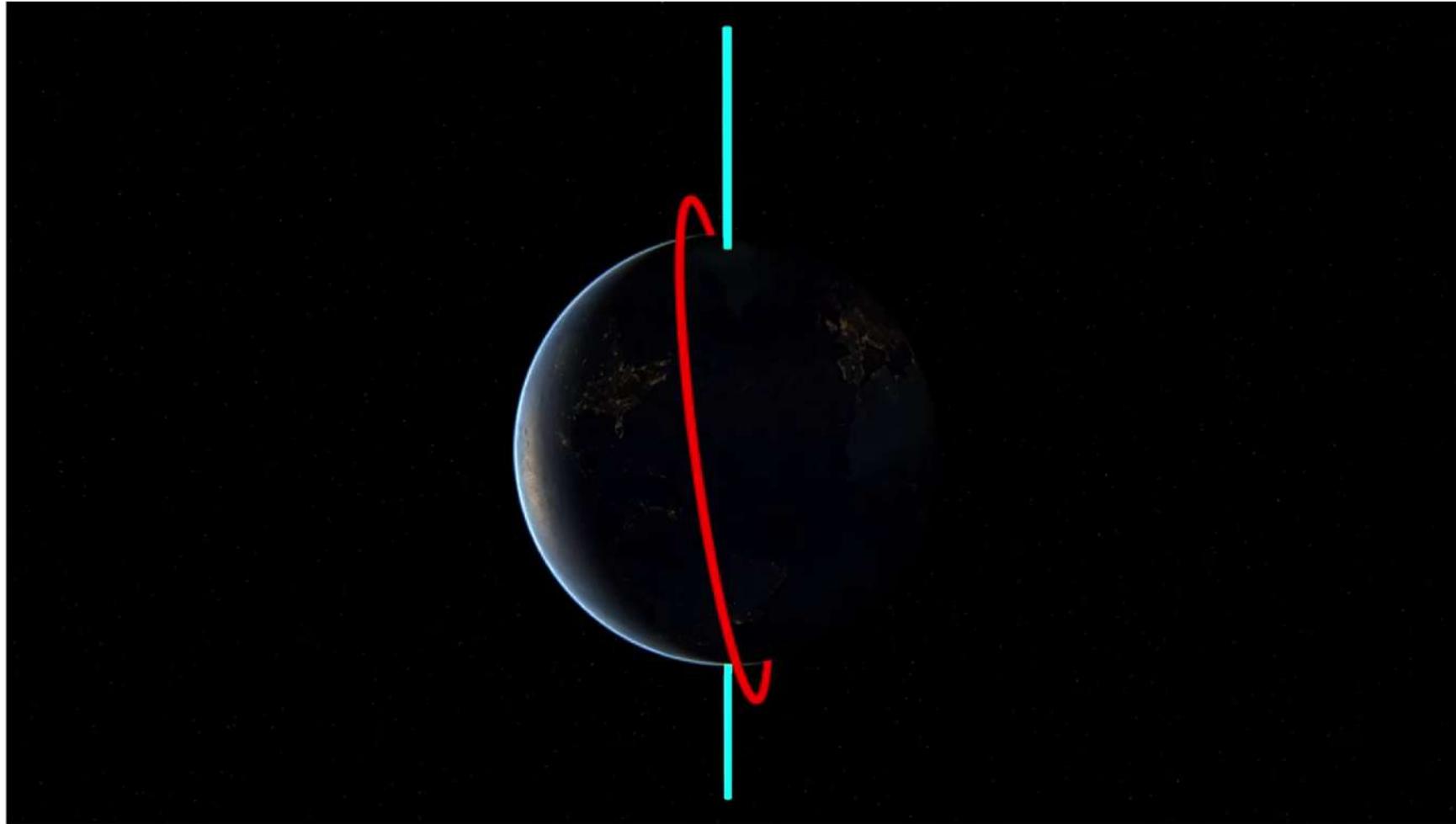


Cubesat analysis “Transient state”

- $\alpha/\varepsilon = 2$; [T = 37.46° C ~ 34.68° C] Steady state Temperature →→
 →→ [T_{moy} = 36.02° C] Initial Temperature injected in Transient analysis

P	1	2	3	4	5	6	7	8	9
Tmax	37.36	37.38	37.39	37.39	37.39	37.39			
Tmin	34.75	34.76	34.77	34.78	34.78	34.78			







Thanks for attending
the presentation



Please feel free to ask
questions

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